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CHARLES RIVER BASIN WESTON, MASSACHUSETTS

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WESTON RESERVOIR DAM MA 00798

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

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DEPARTMENT OF THE ARMY NEW ENGLAND DIVISION, CORPS OF ENGINEERS WALTHAM, MASS. 02154

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IS. SUPPLEMENTARY NOTES

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19. KEY WORDS (Continue on reverse side If necessary and identify by block mamber)

DAMS, INSPECTION, DAM SAFETY,

Charles River Basin Weston, Massachusetts Pine Brook

20. ABSTRACT (Continue on reverse side it necessary and identify by black mamber)

The dam is an earth embankment dam about 1000 ft. long with a maximum height of about 32 ft. It is intermediate in size with a high hazard potential. The dam appears to be in fair condition. The upstream slope appeared to be well maintained and in good condition.

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WESTON RESERVOIR DAM MA 00798

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

NATIONAL DAM INSPECTION PROGRAM

PHASE I INSPECTION REPORT

Identification No.:

MA 00798

Name of Dam:

Weston Reservoir Dam

Town:

Weston

County and State:

Middlesex County, Massachusetts

Stream:

Pine Brook

Date of Inspection:

October 23, 1979

BRIEF ASSESSMENT

Weston Reservoir Dam is an earth embankment approximately 1,000 feet long with a maximum height of about 32 feet. The upstream slope of the embankment is approximately 2H:IV and is protected with heavy cut stone riprap to within two feet of the top of the dam. The downstream slope varies from 2H:IV to 2½H:IV along the length of the dam and the crest of the dam varies from 40 feet to 140 feet in width. The dam was constructed about 80 years ago and it is used as a stand pipe in the Weston Aqueduct which is a portion of the water supply source for the City of Boston and surrounding communities.

The reservoir is located adjacent to Pine Brook which bypasses the reservoir by means of a 36-inch diameter pipe. The bypass pipe conveys the Pine Brook discharge around the left abutment of the dam to a natural stream channel located approximately 200 feet downstream of the dam. The main inflow to the reservoir is from the Weston Aqueduct. The aqueduct terminates upstream of the reservoir and flow from the aqueduct is directed into the reservoir by means of a 100-foot wide, 0.25-mile long channel. Discharge from the reservoir is controlled by a system of 5 stop log bays, which are located in the stone masonry screen chamber and flow control building located about 50 feet to the right of the left abutment. The discharge flows back into the Weston Aqueduct immediately downstream of the screen chamber and flow control building. *A 16-inch low level discharge pipe, located about 500 feet to the left of the right abutment, provides additional discharge capacity. No spillway exists for this structure.

Weston Reservoir has a maximum storage capacity of approximately 1,100 acre-feet, which places the dam in the "Intermediate" size category. Several houses are located within the flood plain of Pine Brook within one mile downstream of the dam. Excessive property damage and loss of life could result in these locations in the event of a dam failure. Therefore, Weston Reservoir Dam is classified in the "High" hazard potential category. The recommended test flood for an "Intermediate" size, "High" hazard dam is the full Probable Maximum Flood (PMF).

The test flood peak inflow to Weston Reservoir was computed to be 1,880 cfs. The routed test flood outflow was computed to be 1,100 cfs and would result in overtopping of the embankment bo 0.5 feet. The reservoir is capable of storing approximately 60 percent of the test flood in surcharge storage prior to overtopping of the embankment.

On the date of the inspection, Weston Reservoir Dam appeared to be in fair condition. The upstream slope appeared to be well maintained and in good condition. However, the downstream slope and, to a lesser extent, the crest of the dam are overgrown with large trees, some as tall as 50 feet. Several roots are exposed along the crest of the dam, indicating the presence of extensive root systems throughout the embankment. In addition, a significant quantity of seepage (5 gpm) was observed approximately 20 feet downstream of the outlet of the 36-inch diameter bypass pipe within a few feet of the downstream toe of the embankment.

Within one year after the receipt of this Phase I inspection report, a qualified registered professional engineer, experienced in the design and construction of dams, should be retained by the Owner for the following purposes: 1) perform a detailed hydrologic and hydraulic study to assess the need for providing spillway discharge capacity; 2) investigate the cause of the seepage within a few feet of the downstream toe of the embankment along the right bank of the stream bypass outlet channel and assess the need for remedial action; 3) investigate the seismic stability of the dam; and 4) direct the removal of the trees from the downstream slope (to a distance of 20 feet downstream of the toe) and crest of the dam to minimize potential damage to the embankment. Voids left in the embankment by the removal of trees should be filled with suitable, thoroughly compacted material.

In addition, the Owner should implement the following operational and maintenance procedures: 1) operability of the low level outlet pipe (16-inch diameter) valve should be investigated, and the valve should be repaired if necessary; 2) develop and implement an ongoing operation and maintenance program; 3) institute a program of annual periodic technical inspection; 4) develop a formal surveillance and flood warning plan, including round-the-clock monitoring during heavy precipitation; and 5) install an upstream closure devise for emergency cutoff of aqueduct flow to the reservoir.

O'BRIEN & GERE ENGINEERS, INC.

John J. Williams) P.E. Vice President

New York Registration N

Date: 24 MANCH 1980

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PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of theses guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation: however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

The Phase I Investigation does <u>not</u> include an assessment of the need for fences, gates, no-trespassing signs, repairs to existing fences and railings and other items which may be needed to minimize trespass and provide greater security for the facility and safety to the public. An evaluation of the project for compliance with OSHA rules and regulations is also excluded.

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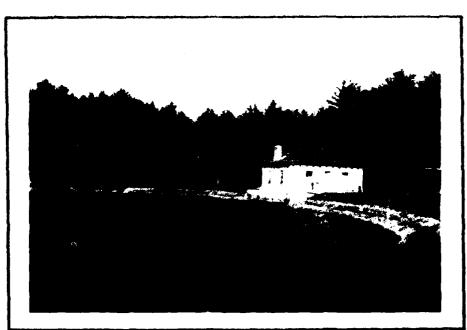
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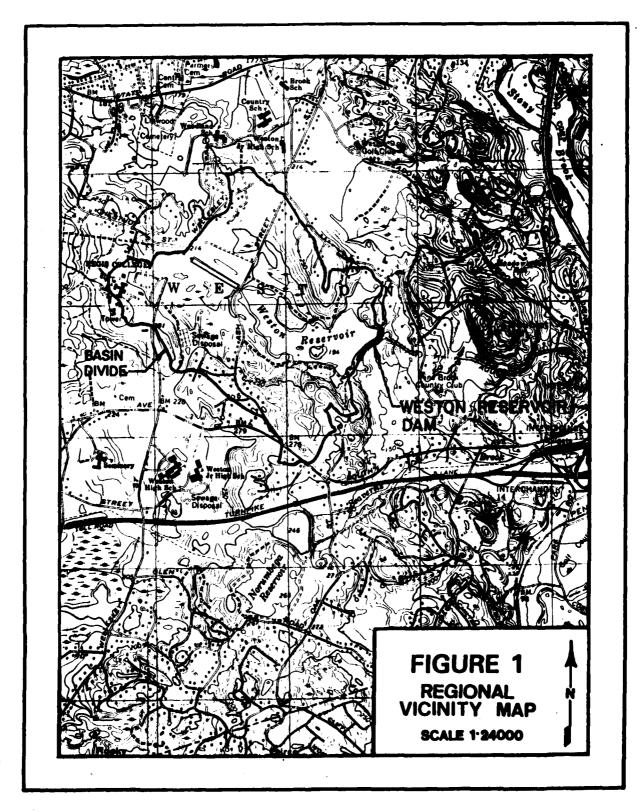
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UPSTREAM OVERVIEW OF WESTON RESERVOIR DAM AS VIEWED FROM THE LEFT ABUTMENT. (10/23/79)



UPSTREAM OVERVIEW OF WESTON RESERVOIR DAM AS VIEWED FROM THE RIGHT ABUTMENT. (10/23/79)



NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT WESTON RESERVOIR DAM

SECTION 1

PROJECT INFORMATION

1.1 General

a. Authority. The National Dam Inspection Act (Public Law 92-367), passed by Congress on August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate the National Program for Inspection of Dams throughout the United States. Responsibility for supervising inspection of dams in the New England Region has been assigned to the New England Division of the Corps of Engineers.

O'Brien & Gere Engineers, Inc. has been retained by the New England Division to inspect and report on selected non-federal dams in the Commonwealth of Massachusetts. Authorization and Notice to Proceed were issued to O'Brien & Gere by a letter dated November 6, 1979 and signed by Colonel William E. Hodgson, Jr. Contract No. DACW33-80-C-0014 has been assigned by the Corps of Engineers for this work.

- b. <u>Purpose of Inspection</u>. The purpose of performing technical inspection and evaluation of non-federal dams is to:
- 1. Identify conditions which threaten public safety and make the Owner aware of any deficiencies so that he may correct them in a timely manner.
- 2. Encourage and prepare the states to initiate effective dam safety programs for non-federal dams as soon as possible.
 - 3. Update, verify and complete the National Inventory of Dams.
- 1.2 <u>Description of Project</u>. (Information with regard to this dam was obtained from Mr. Ray Gaumont, Metropolitan District Commission (MDC) Labor Foreman at Weston Reservoir; the Massachusetts Department of Environmental Quality Engineering (DEQE); and from Mr. Charles Y. Hitchcock, Director and Chief Engineer for the MDC).
- a. Location. Weston Reservoir Dam is located adjacent to Pine Brook in the Town of Weston, Massachusetts. The brook bypasses the reservoir by means of a 36-inch diameter pipe which intercepts the flow from the natural channel upstream of the reservoir, conveys it around the left abutment of the dam and discharges it back to the brook about 200 feet downstream of the dam. Two homes are located on the banks of Pine Brook within a mile downstream of the embankment. Pine Brook flows into Seaverns Brook about a mile downstream of the dam. A portion of the USGS Quadrangle map entitled "Natick, Massachusetts" has been included as Figure 1 on page vi of this report to illustrate the location. USGS coordinates for this dam are N 42°20.3' and W 71°16.6'.

- b. <u>Description of Dam and Appurtenances</u>. Weston Reservoir Dam is an earth embankment approximately 1,000 feet long with a maximum height of 32 feet. The embankment has the following features:
- 1. The upstream face of the embankment has a slope of approximately 2H:IV and is protected by heavy riprap extending from well below the water surface to within about 3 feet of the crest.
- 2. The crest of the dam varies in width from approximately 40 feet at the longitudinal midpoint of the dam to approximately 140 feet at the location of the screen chamber and flow control building which is about 50 feet to the right of the left abutment.
- 3. The downstream slope of the embankment varies within a range of 2H:IV to 2.5H:IV along the length of the dam, with the steeper slope located near the low level discharge pipe.

Outlets from the reservoir include the 16-inch low level discharge pipe located approximately 500 feet left of the right abutment and the Weston Aqueduct which extends from the screen chamber and flow control building in an easterly direction. Page B-3 of Appendix B illustrates the locations of these outlets.

- c. Size Classification. The maximum height of the dam and maximum storage capacity of the reservoir are 32 feet and 1,108 acre-feet, respectively. According to established guidelines, an "Intermediate" size dam is one which is more than 40 feet high (but less than 100 feet high) or has a maximum storage capacity of more than 1,000 acre-feet (but less than 50,000 acre-feet). Therefore, because the reservoir has a storage capacity in excess of 1,000 acre-feet, Weston Reservoir Dam is classified as an "Intermediate" size structure.
- d. Hazard Classification. In general, the area immediately downstream of the dam is sparsely populated. However, there are several houses within one mile downstream of the dam which are within the flood plain. The breach analysis computed a stream depth of 7.3 feet (or 4.3 feet above the channel banks) at the initial damage center 0.6 miles downstream of the dam. This would result in at least 2 feet of water in the first floor of the house at this location. Therefore, loss of life is probable and excessive property damage would be expected. About 1.1 miles downstream, there is a major interchange of the Massachusetts Turnpike which would also be subject to flooding damage as a result of a dam failure. Therefore, Weston Reservoir Dam is classified as a "High" hazard structure.
- e. <u>Ownership</u>. The dam is owned by the Metropolitan District Commission (MDC) located at 20 Somerset Street, Boston, Massachusetts 02109; Telephone 617-727-5275.
- f. Operator. Mr. Ray Gaumont is employed by the MDC at the site to operate the outlet facilities and to maintain the dam.
- g. <u>Purpose of Dam</u>. Weston Reservoir functions as a stand pipe in the Weston Aqueduct which is used as a water supply source for the City of Boston and the surrounding communities.

- h. Design and Construction History: Little information with regard to the design and construction of Weston Reservoir Dam is available. However, a Record Plan dated February, 1905, shows the limits of the core of the dam. A portion of this plan has been included as page B-3 of Appendix B.
- i. <u>Normal Operating Procedures</u>. According to Mr. Gaumont, discharge to the Weston Aqueduct is controlled by inserting or removing stop logs in the five sets of stop log slots located in the screen chamber and flow control building. In addition, debris collected at the screens is removed daily and the screens are cleaned and/or replaced as required.

1.3 Pertinent Data

- a. <u>Drainage Area</u>. The area draining to Weston Reservoir encompasses a 0.9 square mile area to the northwest of the dam in the Town of Weston. The area is primarily wooded and ranges in elevation from 305 to 194 at normal pool level. Several large estates are scattered throughout the watershed.
- b. Discharge at Damsite. (Refer to discharge calculations included in Appendix \overline{D}).
- 1. Outlet Works. A 16-inch low level outlet is located approximately 500 feet left of the right abutment, as shown on page B-3 of Appendix B. If the low level discharge valve is operable, this outlet may be used to lower the water level in the reservoir. Outflow through the screen chamber and flow control building to the aqueduct downstream was assumed equal to the inflow to the reservoir from the aqueduct upstream.
 - 2. Maximum Known Flood. Flood records are not kept for this site.
 - 3. Ungated Spillway Capacity at Top of Dam. Not Applicable.
 - 4. Ungated Spillway Capacity at Test Flood Elevation. Not Applicable.
 - 5. Gated Spilway Capacity at Normal Pool Elevation. Not Applicable.
 - 6. Gated Spillway Capacity at Test Flood Elevation. Not Applicable.
 - 7. Total Spillway Capacity at Test Flood Elevation. Not Applicable.
- 8. Total Project Discharge at Top of Dam. No spillway has been provided for this structure. Therefore, the only discharge from the reservoir is through the screen chamber and flow control building and into the aqueduct (assumed equal to the inflow from the aqueduct) or through the low level blow-off pipe.
- 9. Total Project Discharge at Test Flood Elevation. At the test flood elevation of 201.5, the discharge over the top of the dam was computed as 1,100 cfs.

С.	<u>Ele</u>	vation. (NGVD)	
	1. 2. 3. 4. 5. 6. 7. 8. 9.	Streambed at Toe of Dam Bottom of Cutoff Maximum Tailwater Normal Pool Full Flood Control Pool Spillway Crest (Gated) Design Surcharge (Original Design) Top of Dam Test Flood Design Surcharge	169 Unknown NA 194 NA NA Unknown 201 201.5
d.	Res	<u>ervoir Length</u> . (Feet)	
	1. 2. 3. 4. 5.		4,000 NA NA 4,700 4,750
e.	Sto	rage. (Acre-feet)	
	1. 2. 3. 4. 5.	Normal Pool Flood Control Pool Spillway Crest Pool Top of Dam Test Flood Pool	486 NA NA 1,108 1,174
f.	Res	ervoir Surface. (Acres)	
	1. 2. 3. 4. 5.	Flood Control Pool	61 NA NA 120 122
g.	Dam	1	
	1. 2. 3. 4. 5.		Earth Embankment 1,000 feet 32 feet Varies, 40 feet to 140 feet Upstream 2H:IV Downstream 2H:IV - 2½H:IV Unknown Unknown Yes, but composition Unknown
	9.	Grout Curtain	Unknown

h. <u>Diversion and Regulating Tunnel</u>.

1. Type 36-inch diameter reinforced concrete pipe
2. Length 2,500 feet
3. Closure None
4. Access Manhole
5. Regulating Facilities None

i. Spillway.

None

j. Regulating Outlets.

1. Weston Aqueduct
a) Invert
b) Size
9.25 feet high by 10 feet
(minimum)

c) Description Weston Aqueduct
d) Control Mechanism Stop logs

2. Low Level Discharge Pipe
a) Invert at Outlet 169.0+
b) Size 16 inches
c) Description Cast iron pipe
d) Control Mechanism Unknown

SECTION 2

ENGINEERING DATA

2.1 Design

No design information for Weston Reservoir Dam is available, according to Mr. Ray Gaumont, MDC Labor Foreman employed at the site.

2.2 Construction

Record drawings of the reservoir indicate that the dam was constructed about 1900. These same drawings indicate the presence of a core wall for the entire length of the dam. A portion of the drawings have been included in Appendix B.

2.3 Operation

Operating procedures include installation and removal of stop logs to control the amount of water discharged to the Weston Aqueduct. The stop logs are normally not used. Only when the MDC wants to shut down the Weston Aqueduct are the stop logs used.

2.4 Evaluation

a. Availability.

- 1. The record drawings, topographic plans, and information about the Weston Aqueduct were obtained from the MDC.
- 2. An inspection report for Weston Reservoir Dam, dated 1/17/74, was obtained from the Massachusetts DEQE, 100 Nashua Street, North Station, Room 532, Boston, Massachusetts, 02114.
- 3. In addition, operating information was obtained during the visual inspection and from subsequent telephone conversations with Mr. Ray Gaumont, the MDC Labor Foreman employed at the site (617-893-7499).
- b. <u>Adequacy</u>. The information provided by MDC, DEQE, and Mr. Gaumont combined with the information obtained during the visual inspection is considered adequate for a Phase I evaluation.
- c. Validity. The record drawings and other information obtained from the MDC appear to be valid. The DEQE inspection report, however, included inspection of only a small portion of the dam at the screen chamber and flow control building (referred to as the granite block pump station in the DEQE inspection report). Consequently, the DEQE report does not accurately define the dam, which is actually an estimated 1,000 feet long and 32 feet high with a top width varying between approximately 40 and 140 feet. The DEQE report states that the dam is 80 feet long, 27 feet high and has a top width of 3 feet. The possible consequences of a dam failure can not be accurately predicted using the information in the DEQE report. A copy of the DEQE inspection report has been included as pages B-6 through B-11 in-Appendix B.

SECTION 3

VISUAL INSPECTION

3.1 Findings

a. <u>General</u>. Weston Reservoir Dam was inspected on October 23, 1979. At the time of inspection, the pool elevation was approximately 7 feet below the top of the dam. No underwater areas were inspected.

Observations and comments made during the field inspection appear on a checklist included as Appendix A of this report.

b. Dam. The upstream face of the embankment appears to be well maintained and in good condition. A 30-foot wide strip along the upstream edge of the dam crest is grass-covered and appears to be well maintained. However, the remainder of the crest of the embankment is covered with large trees, some as tall as 50 feet. The downstream face of the dam is overgrown with large trees with trunks up to 2 feet in diameter and heights up to 50 feet which partially obscure the condition of the embankment.

Clear seepage (estimated at 5 gpm) was observed discharging from the right channel bank of the stream approximately 20 feet downstream of the outlet of the bypass conduit within a few feet of the embankment toe.

Sections and photographs of the dam are included in Appendix B and Appendix C, respectively.

c. Appurtenant Structures. The screen chamber and flow control building located near the left abutment which contains chlorination facilities and provides access to the inlet screens appears to be in good condition. The five stop log bays located in the lower portion of the screen chamber and flow control building appear to be in good condition. Control of the discharge from Weston Reservoir to the Weston Aqueduct is provided through the insertion or removal of stop logs in the stop log bays.

The 16-inch pipe located about 500 feet left of the right abutment which functions as the low level outlet for the reservoir appears to have not been used in many years. The outlet and discharge channel for the low level outlet pipe are almost impossible to discern in the forest litter and underbrush. The Owner's representative could not give us any information concerning the control mechanism for the low level outlet.

d. Reservoir Area. The reservoir shoreline has slopes varying from 1 to 20 percent. The area draining to Weston reservoir is primarily comprised of forested and swampy land with several large residences within the Town of Weston. Evidence of slope instability or reservoir siltation was not observed.

e. <u>Downstream Channel</u>. A 36-inch concrete pipe intercepts Pine Brook to the north of the reservoir and conveys it around the left abutment of the dam and back to its natural stream channel about 200 feet downstream of the dam. From this point Pine Brook conveys the water southeasterly to Seaverns Brook about 1.0 miles downstream of the dam and ultimately to the Charles River about 1.5 miles downstream of the dam. Several homes are located within the flood plain within the first mile downstream of the dam.

The only direct discharge from the reservoir enters the Weston Aqueduct at the downstream end of the screen chamber and flow control building and is conveyed towards the Chesnut Hill Reservoir and eventual distribution in the City of Boston.

3.2 Evaluation

The upstream face of the embankment appears to be well maintained and is provided with heavy stone riprap for erosion protection. The upstream portion of the crest is also well maintained and grass-covered. However, the downstream face of the embankment and downstream portion of the crest are overgrown with large trees which hinder a detailed inspection of the embankment condition. In addition, the trees create a hazard to the integrity of the embankment by virtue of their apparently extensive root systems. The roots of the larger trees create potential seepage paths through the embankment and should any of these trees be uprooted during severe wind conditions, a significant amount of embankment material would be displaced.

Another matter of concern is the approximately 5 gpm of seepage observed on the right bank of the bypass outlet channel about 20 feet downstream of the outlet on the 36-inch pipe within a few feet of the embankment toe. Further investigation of this seepage is recommended.

Several photographs of the dam have been included in Appendix C to illustrate the conditions described above.

SECTION 4

OPERATIONAL AND MAINTENANCE PROCEDURES

4.1 Operational Procedures

- a. <u>General</u>. The only operational procedure performed at the site is the infrequent insertion or removal of stop logs to regulate reservoir discharge to the aqueduct.
- b. <u>Description of Any Warning System in Effect</u>. According to Mr. Gaumont, the Owner's representative, there is no downstream warning system in effect at this site.

4.2 Maintenance Procedures

- a. General. According to the Owner's representative, other than daily removal of debris collected on the screens at the inlet to the screen chamber and flow control building and periodic mowing of the upstream side of the dam crest, no maintenance tasks are performed on a routine basis. Other maintenance tasks are performed, as the need arises, by a MDC crew employed at the site.
- b. <u>Operating Facilities</u>. The screen chamber and flow control building contains chlorination facilities for the reservoir and provide access to the inlet screens and stop log slots. According to the Owner's representative, there are no routine maintenance procedures other than those discussed in the preceding subsection.

4.3 Evaluation

The current maintenance program has provided for care of the grounds and screening facilities. However, the program has not provided procedures for proper maintenance of the dam crest and the downstream face of the dam which should be kept clear of trees, brush, etc.

SECTION 5

EVALUATION OF HYDRAULIC/HYDROLOGIC FEATURES

5.1 General

The drainage area to Weston Reservoir is approximately 0.9 square miles of relatively hilly, wooded, swampy terrain in the Town of Weston. The drainage area is sparsely populated, with only a small number of residences throughout the basin. The topography ranges from Elev. 305 in the upper reaches of the watershed to Elev. 194 at the normal pool water surface. A 36-inch bypass pipe intercepts the discharge of Pine Brook north of the reservoir and conveys it to Pine Brook about 200 feet downstream of the dam. Upstream of the reservoir, Weston Aqueduct discharge flow into a 100-foot wide, 0.25-mile long channel which directs the flow into Weston Reservoir. Discharge from the reservoir travels through the screen chamber and flow control building and into the aqueduct which resumes its course immediately downstream of the dam. No spillway is provided for this structure for additional discharge capacity.

5.2 Design Data

According to the Owner's representative, no hydraulic or hydrologic design data is available.

5.3 Experience Data

Reservoir pool elevation records have been maintained by the MDC and are available at the site and at their main office in Boston. According to MDC personnel, the embankment has never been overtopped.

5.4 Test Flood Analysis

The recommended test flood for an "Intermediate" size, "High" hazard dam is the full Probable Maximum Flood (PMF).

Hydrologic and hydraulic calculations were performed with the assistance of the HEC-1-DB computer program. The flood hydrographs were constructed from the Snyder unit hydrographs using average coefficients, an initial infiltration of zero and a constant loss rate of 0.05 inches per hour. The Hop Brook Adjustment Factor was used to reduce the Probable Maximum Precipitation (PMP) based on the drainage area. A Stage vs. Storage relationship was developed for Weston Reservoir. This relationship was utilized by the program to route the test flood through the dam. Inflow from the upstream aqueduct was assumed equal to outflow to the downstream aqueduct so that the only project discharge was due to flow over the top of the dam. The reservoir water surface was assumed to be at the normal pool elevation of 194 at the beginning of the storm event.

The test flood peak inflow to Weston Reservoir Dam was computed to be 1,880 cfs. The routed test flood outflow was computed to be 1,100 cfs which would result in overtopping of the embankment by 0.5 feet. The reservoir is capable of retaining approximately 60 percent of the test flood in surcharge storage prior to overtopping of the embankment.

5.5 Dam Failure Analysis

A failure of the embankment was simulated by the HEC-1-DB computer program assuming a 400-foot wide and 26-foot deep breach with vertical side slopes developing within 3 hours. The failure is assumed to occur with the reservoir surface at the top of dam elevation. The resulting outflow was routed to the potential damage center, which was assumed to be the first house approximately 0.6 miles downstream on the banks of Pine Brook. The channel cross-section at this point is shown on page D-3. The increase in stream depth at this location was computed to be 7.3 feet, or 4.3 feet above the banks of the channel with a maximum flow of 8,830 cfs. This would result in at least 2 feet of water in the house 0.6 miles downstream of the dam. Excessive property damage and possibly the loss of several lives could occur.

SECTION 6

EVALUATION OF STRUCTURAL STABILITY

6.1 Visual Observations

At the time of inspection, no signs of settlement, cracking, or other structural movement were observed. The upstream face and crest of the dam are well maintained and appeared to be in good condition. The downstream face of the embankment and a portion of the dam crest are partially obscured by a heavy growth of trees, brush and forest litter; therefore, it is difficult to tell if the downstream face of the dam and the crest are free of structural deficiencies. The root systems of the trees create a potential hazard to the integrity of the embankment. Severe winds could uproot some of the trees, thereby dislodging portions of the embankment in the process. The root systems of the trees could also create seepage paths through the dam.

During the inspection, significant seepage (approximately 5 gpm) was observed about 20 feet downstream of the 36-inch bypass pipe outlet along the right side of the outlet channel within a few feet of the downstream embankment toe. Seepage of this magnitude could endanger the stability of the structure due to the possibility of migration of fine material through the embankment.

6.2 Design and Construction Data

Little information with regard to the original design and construction of the dam is available. A portion of the record plans are included in Appendix B. No indication of materials used in the construction of the dam or core wall is given on the plans and no specifications are available.

6.3 Post Construction Changes

There are no known modifications to the original construction of the $\mbox{dam.}$

6.4 Seismic Stability

Weston Reservoir Dam is located in Seismic Zone 3 on the "Seismic Zone Map of Contiguous States." Therefore, according to the Recommended Guidelines for Phase I Safety Inspection of Dams, a seismic stability analysis should be performed as recommended in Section 7.

SECTION 7

ASSESSMENT, RECOMMENDATIONS & REMEDIAL MEASURES

7.1 Dam Assessment

- a. <u>Condition</u>. Based upon the visual inspection, Weston Reservoir Dam appears to be in fair condition. The upstream face of the dam and the portion of the dam crest nearest the reservoir appear to be in good condition. Two conditions at the site, however, present some cause for concern. Trees and brush on the crest and downstream face of the embankment pose a potentially dangerous situation, as discussed in Sections 3.2 and 6.1, and seepage about 20 feet downstream of the outlet of the stream bypass pipe within a few feet of the downstream embankment toe.also poses a potentially dangerous situation.
- b. <u>Adequacy of Information</u>. The information obtained from the MDC, DEQE, and Mr. Gaumont, combined with the information obtained during the field investigation, is considered adequate for a Phase I evaluation.
- c. Urgency. The recommendations and remedial measures described in Sections $\overline{7.2}$ and 7.3 should be implemented within one year from the date of receipt of this report.

7.2 Recommendations

- It is recommended that the Owner retain the services of a qualified registered professional engineer, experienced in the design and construction of dams, for the following purposes:
- 1. Perform a detailed hydrologic and hydraulic study to assess the need for providing spillway discharge capacity.
- 2. Investigate the cause of the seepage within a few feet of the downstream toe of the embankment along the right bank of the stream bypass outlet channel and assess the need for remedial action.
- 3. Investigate the seismic stability of the dam utilizing conventional equivalent static load methods.
- 4. Direct the removal of the trees from the downstream face (to a distance of 20 feet downstream of the toe) and crest of the dam to minimize damage to the embankment. Voids left in the embankment by the removal of trees should be filled with suitable, thoroughly compacted material.

7.3 Remedial Measures

- a. Operation and Maintenance Procedures. The Owner should also implement the following operation and maintenance measures:
- Operability of the low level outlet pipe (16-inch diameter) valve should be investigated, and the valve should be repaired if necessary.
- 2. Develop and implement an ongoing operation and maintenance program to insure the future integrity of the dam.
 - 3. Institute a program of annual periodic technical inspection.
- 4. Develop a formal surveillance and flood warning plan, including round-the-clock monitoring during heavy precipitation.
- 5. Install an upstream closure device for emergency cutoff of aqueduct flow to the reservoir.

7.4 Alternatives

No valid alternatives to the recommendations described above are considered feasible for this site.

APPENDIX A

INSPECTION CHECKLIST

VISUAL INSPECTION CHECK LIST

INSPECTION TEAM ORGANIZATION

Project:	Weston Reservoir Dam	
National I.D. #:	MA 00798	
Location:	Weston, Massachusetts	
Type of Dam:	Earth Embankment	
Inspection Date(s):	October 23, 1979	
Weather:	Partly Cloudy, 70	
Pool Elevation:		
Inspection Team		
Leonard Beck Steven Snider Alan Hanscom Rodney Georges	O'Brien & Gere O'Brien & Gere O'Brien & Gere Bryant & Associates	Structures Foundations & Materials Structures Hydrology/Hydraulics
*Mr. John J. Williams, Vi necessarily in conjunction	ce-President, O'Brien & Ge with the inspection team.	ere has visited the site but not
Owner's Representative	1	
Mr. Ray Gaumont, MDC	Labor Foreman	
	·	

	VISUAL INSPECTION CHECK LIST
Project:	Weston Reservoir Dam
National I.D. #:	MA 00798
Date(s):	October 23, 1979

AREA EVALUATED	CONDITIONS
DAM EMBANKMENT	
Crest Elevation (Ft. above MSL)	204 <u>+</u>
Current Pool Elevation	197 <u>+</u>
Maximum Impoundment to Date	Unknown .
Surface Cracks	None Observed
Pavement Condition	N/A
Movement or Settlement of Crest	None Observed
Lateral Movement	None Observed
Vertical Alignment	Appears to be good
Horizontal Alignment	Appears to be good
Condition at Abutment and at Concrete Structures	Good
Indications of Movements of Structural Items on Slopes	None Observed
Trespassing on Slopes	Negligible
Vegetation on Slopes	Heavy growth on d/s slope u/s slope mowed
Sloughing or Erosion of Slopes or Abutments	Slight undulations @d/s to
Rock Slope Protection - Riprap Failures	No failures Observed

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	VISUAL INSPECTION	ON CHECK LIST
Project:	Weston Reservoir	Dam
National I.D. #:	MA 00798	
Date(s):	October 23, 1979	·
AREA EVA	LUATED	CONDITIONS
DAM EMBANKMENT (Con't)	
Unusual Movement o	or Cracking at or near Toes	Undulations
Unusual Embankmen	t or Downstream Seepage	∼5gpm Seepage @ toe near outlet of bypass
Piping or Boils		None Observed
Foundation Drainage	: Features	Unknown
Toe Drains		Unknown
Instrumentation Syst	:em	N/A
	·	
		. ,
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VISUAL INSPECTION CHECK LIST Project: Weston Reservoir Dam MA 00798 National I.D. #: Date(*): 0ctober 23, 1979 **AREA EVALUATED** CONDITIONS OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DISCHARGE CHANNELS Approach Channel Not Applicable **General Condition** Not Applicable Not Applicable Loose Rock Overhanging Channel Trees Overhanging Channel Not Applicable Floor of Approach Channel Not Applicable Weir and Training Walls Not Applicable Not Applicable General Condition of Concrete Not Applicable Rust or Staining Not Applicable Spalling Not Applicable Any Visible Reinforcing Any Seepage or Efflorescence Not Applicable **Drain Holes** Not Applicable Discharge Channel General Condition Overgrown with brush n≈ 0.045

	VISUAL INSPECTION	CHECK LIST
Project:	Weston Reservoir Da	nm
National I.D. #:	MA 00798	
Date(s):	October 23, 1979	
AREA EVAL	UATED	CONDITIONS
OUTLET WORKS - SPILL AND DISCHARGE CHA	WAY WEIR, APPROACH ANNELS (Con't)	
Loose Rock Overh	anging Channel	In a few places
Trees Overhanging	g Channel	Several Small trees
Floor of Channel		Rough w/stones & debris
Other Obstruction	s	Downstream culvert

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VISUAL INSPECTION CHECK LIST	
Project: Weston Reservoir Dam	
National I.D. #: MA 00798	
Date(s): October 23,1979	
AREA EVALUATED	CONDITIONS
OUTLET WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE	
a. Approach Channel	Not Applicable
Slope Conditions	Not Applicable
Bottom Conditions	Not Applicable
Rock Slides or Falls	Not Applicable
Log Boom	Not Applicable
Debr is	Not Applicable
Condition of Concrete Lining	Not Applicable
Drains or Weep Holes	Not Applicable
b. Intake Structure	
Condition of Concrete	Good
Stop Logs and Slots	For (5) inlet gates ~ good condition

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VISUAL INSPECTION CHECK LIST Weston Reservoir Dam Project: National I.D. #: MA 00798 Date(s): 0ctober 23,1979 **AREA EVALUATED** CONDITIONS **OUTLET WORKS - OUTLET STRUCTURE AND** OUTLET CHANNEL General Condition of Concrete Good @ structure -Aqueduct Unknown Rust or Staining None Observed Spalling Slight **Erosion or Cavitation** None Visible Reinforcing None Any Seepage or Efflorescence None at Aqueduct Condition at Joints Unknown **Drain Holes** None Observed Channel N/A N/A Loose Rock or Trees Overhanging Channel N/A Condition of Discharge Channel

<u> A-7</u>

VISUAL INSPECTION CHECK LIST		
Project:_	Weston Reservoir Dam	
National I.D. #:	MA 00798	
Date(s):	October 23, 1979	

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APPENDIX B

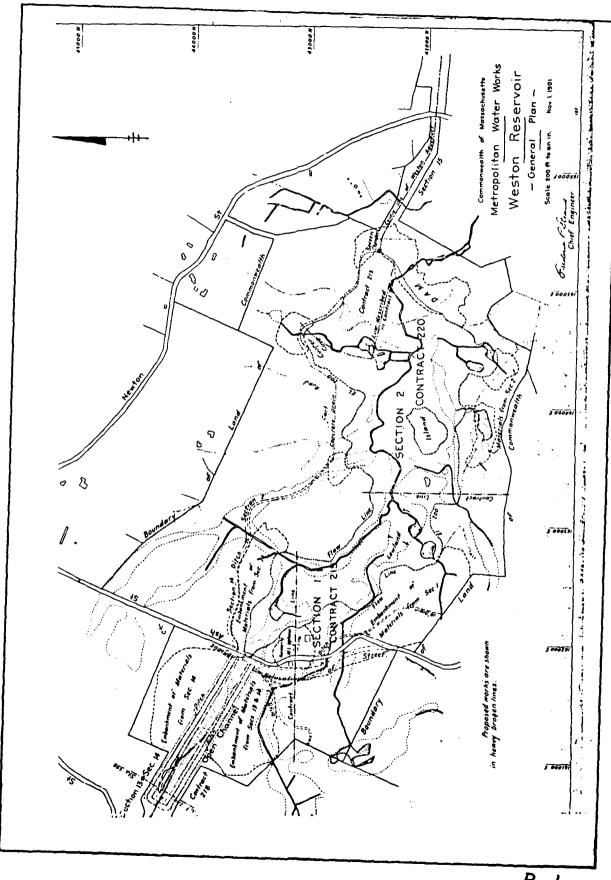
ENGINEERING DATA

APPENDIX B

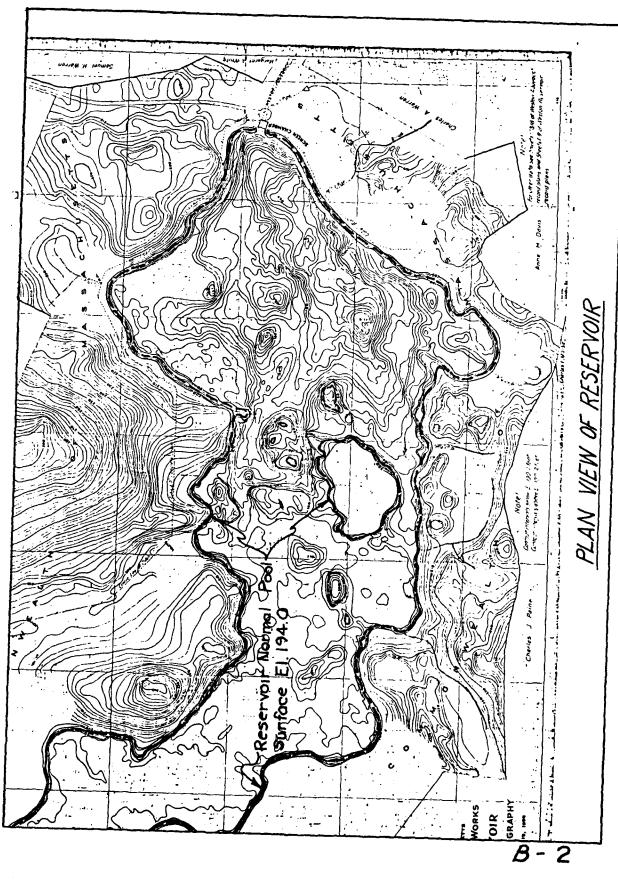
ENGINEERING DATA

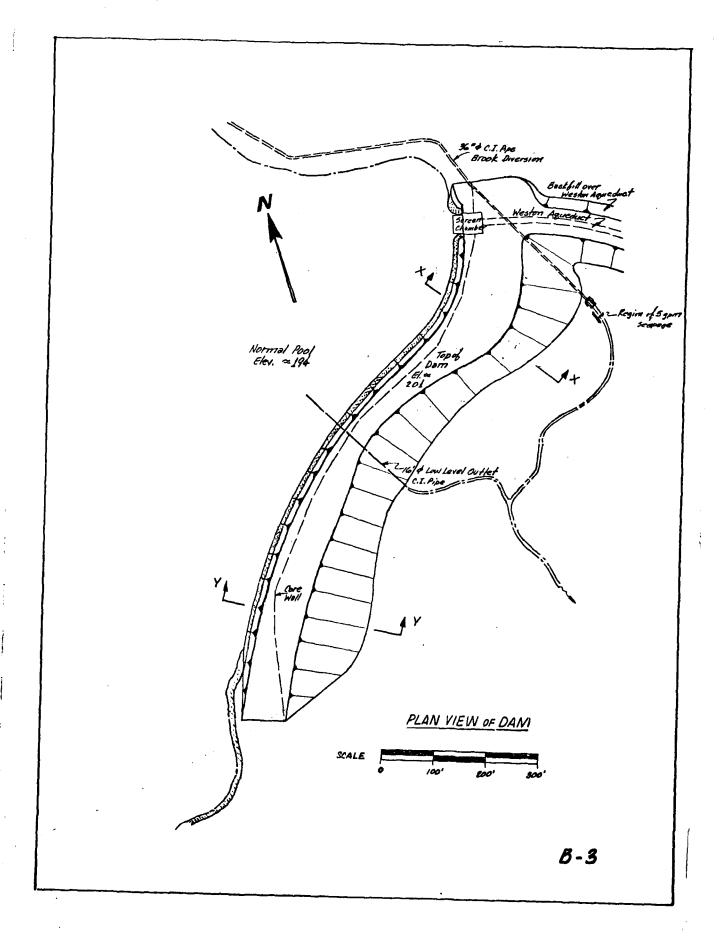
TABLE OF CONTENTS

	PAGE
GENERAL PLAN 1901	B-1
PLAN VIEW OF RESERVOIR	B-2
PLAN VIEW OF DAM	B-3
EMBANKMENT SECTIONS	B-4
WESTON AQUEDUCT	B-5
COMMONWEALTH OF MASSACHUSETTS INSPECTION REPORT	8-6 Thru 8-11



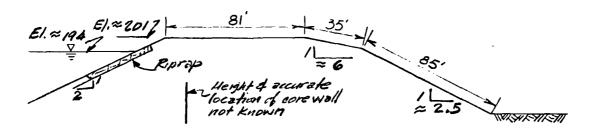
B- 1



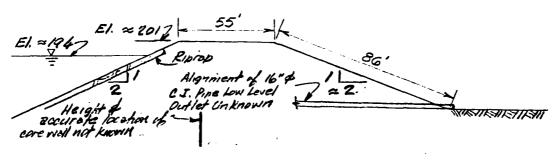




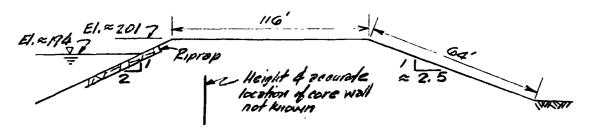
SUBJECT WESTON RESERVOIR DAM SHEET BY 3/3/80 2060-001



SECTION Y-Y = 200' NORTH OF SOUTH ABUTMENT



SECTION AT LOW LEVEL OUTLET

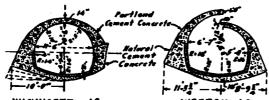


SECTION X-X 200' SOUTH OF NORTH ABUTMENT

EMBANKMENT SECTIONS

Scale: |"= 50"

B-4



WACHUSETT 1: 2500



MAIN SUDBURY AQ. GRAPE 1:5280

WESTON AQ.

M.D.C. WATER DIVISION AQUEDUCTS

UPPER PORTION GRAFE I: SECO



SUDBURY SUPPLY AQ

WESTON AQUEDUCT

Built by Metropolitan Water Works. First used in December 1905. Capacity, 300,000,000 gallons in 24 hours
Capacity, 300,000,000 gallons in 24 hours
Subbury Damto Head House: 4702' of 2 lines 60 CI.Pipe
Head House to siphon under N.V., N.H. & H.R.R. ot
Nobscot: concrete equedact, fell of 14.48' or 4.224'
o mile, size 10'-0" wide at springing linex 3.2' high
for 3.45 miles. S:1:1250 TOT 0.95 MIVES, 5:1:1250
Siphon under NY, N.H.H.R.R. of Nobsed:1302'ling, full 2:22
Siphon of Nobseet to Chamber: Fell of 10.5 7'
or 1.056' o mile, size 13.17 mide at springing line
#1217' high for 7.79 miles 5:1:5000
Yotal length 13.42 miles:

STATUS MILES INVERT Head House (and of pipes, entrance to Read House) 5+06 215.89 Tunnel Ma. I (beginning) Gaging (beamber Ma.) Townel Ma.2 (beginning) Turnel No. 3 (beginning) 7400 17400 0.2 214.97 42-30 0.7 212.96 N3+20 2.0 Makscot Siphon (beginni) Makscot Siphon (end) Gaging Chomber No. 2 196-59 34 201.41 187+80 85 |98.49 214:121 £0 |97.97 or Chambel Bryin of Sud Liv. Siphord 284-98 53 196.94 Chamber Ma. 2 (oud -- --) 320-74 6.0 194.15 hon Chamber Na. 2 lend ... Sphon Chamber Mo. 2 (and "" | 920170 68 179.15
Sphon Cham Mo. 5 (begin, all Appy Hollon Sphoid 5347 68 193.46
Sphon Cham Mo. 4 (beginning) | 92946 10.0
End of Aquedoct, (Channel Chamber) | 597080 113 187.92
Ash St. Bridge, Last End | 649180 123 187.50
Serven Chamber, West End | 649180 123 187.50
Terminal Chamber (end of aquedoct) | 706-99 16.42 187.50
Enfrance to Distributing Pipes | 706-99.44 187.50 15444)153453 66 1100--) 384077 68 192.57

"Sodbury Liver Sighon crosses the river by arching the pipe to corry itself and the weight of the water; rise of pipe 5.5 ft; length beforem abotements 20.0 ft. "Open Channel is 11 g miles from Sudbury Dam and is 1400" leng. 12 deep f 16 vide et bottom, object sides 5:1 Double Station at 550.74 book and 5 to 450 ahead - 416 - 70 " 416155 "

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	3. Rame	St. & no.	City	/Tom	State	fel. no.
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S	. Colonia Train and Tracally Williams whereas alternate	taket kon <u>Nune</u> .		managhir da ramak e		
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	3. Severe		4. D	isastrons	***	•
	* This rating may	change as land use ch	d erutura) Begne	nekijoleve	(s)	
(6.)	Outlet Control:	Automatio	. Kang	થે		•
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	Commands	M.D.C. Wa	ter sun	1/4	line 15	74 p
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مرادات مستحدات						
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		_ 3. Waj	or Repairs	. 4	. Urgent Rep	airs
	Comments	:				
			ran kathatan ana santan ay ay ay ay ana ar ata ar a	-		
						8.6

1.

(8)	DAM NO. 4-9-333-4 Downstream Face of Dam: Condition: 1. Good 2 Minor Repairs		
	3. Major Repairs Urgent Repairs Comments:		
(9)	Emergency Spillway: Condition: 1. Good 2. Minor Repairs 4. Urgent Repairs		
	Comments:		
(10)	Water level @ time of inspection 5 ft. above below		
•	top of dam / Principal spillway		
	other		
(11)	Summary of Deficiencies Noted:		
:	Growth (Trees and Brush) on Embankment		
	Animal Burrows and Washouts		
į	Damage to slopes or top of dam		
ī	Cracked or Damaged Masonry		
	Evidence of Seepage		
1	Evidence of Piping		
	Erosion		
1	Leaks		
:	Trash and/ar debris immeding flow		
	Clogged or blocked spillway		
Į.	Other		

(12.)

Remarks & Recommendations: (Fully Emplain)

OAM EN (roop condition)

***		SON CONTROL OF CONTROL
(13.)	Overall Condition	ons:
	1.	Safe V
	z.	Minor repairs needed
	3.	Conditionally safe - major repairs meaded
	1	Unselo
	5.	Reservoir impoundment no longur exists (emploin)
		Rosouristed removal from inspection list

DESCRIPTION OF DAH DISTRICT_14

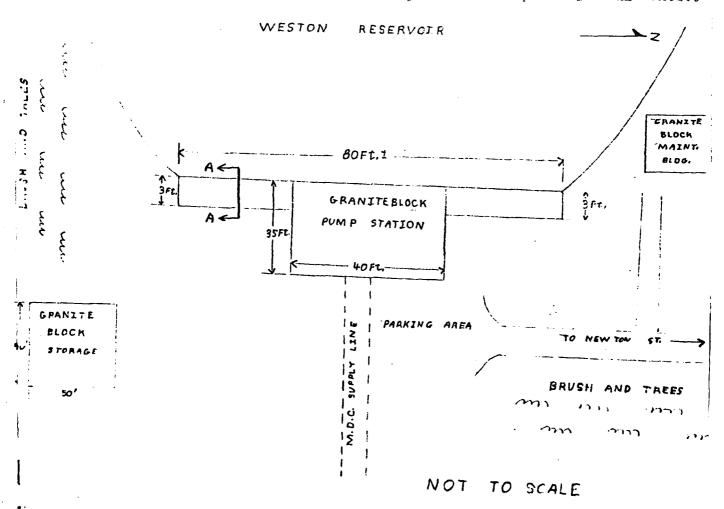
Sub Dad	in JAN. 17 19 74	Dam No. 4-9-333-4 City/Town Lives Tola Name of Dam Wester Reserved
\$.	Location: Topo Shaot No. 2.6.0 Provide 80 x 210 in clear copy of topo map clearly indicated.	with location of Dam
2,	Year built: Year/s of subsequent re	palrs
3.	Percora of Dea: Water Supply	creationalher
ķ.	Drilinuge Avea:	5.60 acres.
5.	Remari Pending Area: 60 acros: Ave Depth	101=tacre ft.
8.	No. and type of dwellings located adjacent to 1 of support horses etc. One block lump Houses	pond or reservoir
1.	Birensions of Dem: Langth <u>30Ft, t</u> Max. He Signes: Upstream Face <u>Verlinal</u> Bovestiedin Face <u>Verlinal</u> Width across top <u>3Ft</u>	r I ical
8.	Classifications of Pam by Materials: Serch Conc Masonary V Timber Reckfill	Stone MasonaryOther
\$	A. Decompains of present land usage downstee 5 On hon it chart a storage wreams in flood plain dot 1.0 m in the incompany diment in the orent on n	wastreem of dem: which could

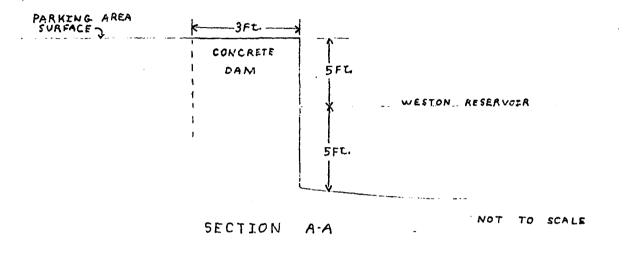
10. hisk to life and property to every of complete failure.

No. of people NoNE
No. of homes NONE
No. of businesses NONE
No. of industries NONE
No. of utilities ONE
Railroads NONE
Other dams NONE

Type M. D.C. water supply line + pring he

Abtach skepch of dam to 20 s form showing rection and plan 83° x 11° Sheet.



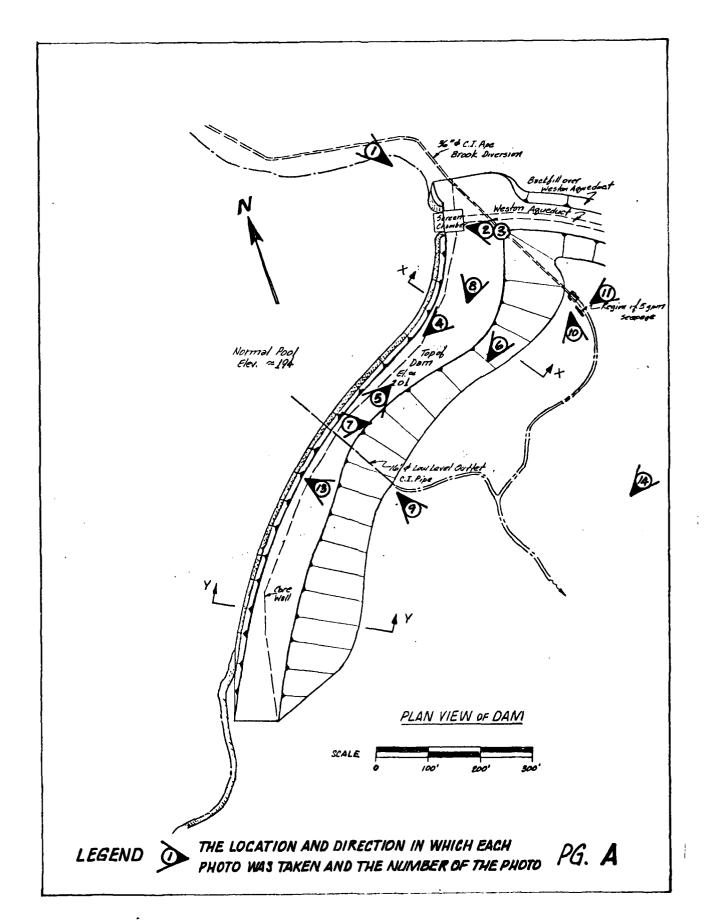


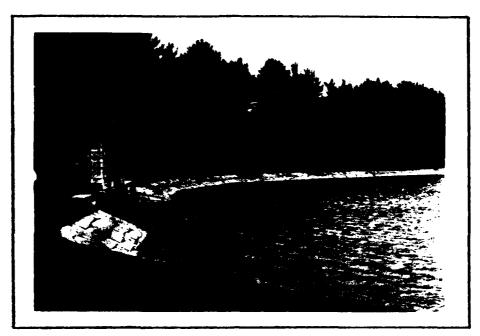
APPENDIX C

PHOTOGRAPHS

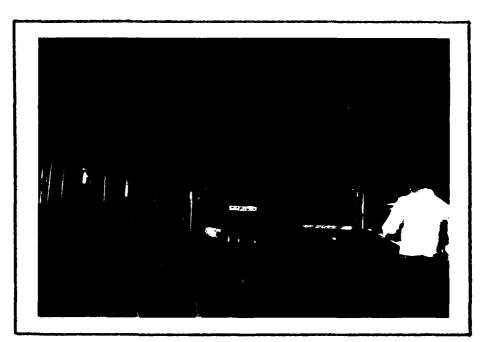
APPENDIX C SELECTED PHOTOGRAPHS OF PROJECT

LOCA	TION PLAN	Page No.
Site	Site Plan Sketch	
PHOT	OGRAPHS	
No.		Page No.
1.	Gatehouse and upstream slope	1
2. 3.	Gatehouse interior showing mechanical stop log hoist Inlet portal and trash screen in gatehouse	1 2
4.	Riprap on upstream slope, grass cover and large trees on the dam.	2
5.	Close up of large trees growing on the dam crest and downstream slope.	3
6.	Downstream slope of the dam showing large trees and undergrowth.	3
7.	50 foot tall trees on the dam crest and downstream slope.	4
8.	Large tree root on the dam crest.	4
9.	Outlet of 16 inch diameter cast iron pipe reservoir blow-off.	5
10.	Outlet of 36 inch diameter stream by-pass conduit at the downstream toe of slope of the dam.	5
11.	5 g.p.m. seepage from the downstream toe of slope of the dam along the stream by-pass outlet channel.	6
12.	Intake canal connecting the aqueduct with Weston Reservoir.	6
13.	Weston Reservoir as viewed from Weston Reservoir Dam.	7
14.	Golf course through which discharge channel flows from approximately 200 to 900 yards downstream of the dam.	7
15.	Potential hazard area about 1200 yards downstream from the dam.	8
16.	Potential hazard area about 1400 yards downstream from the dam.	8





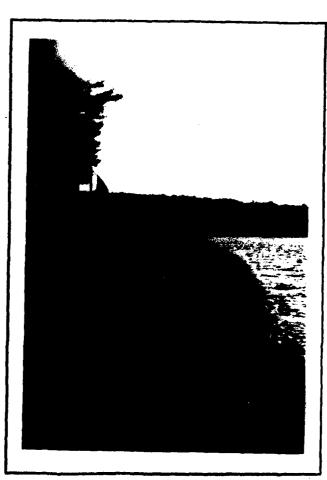
1. GATEHOUSE AND UPSTREAM SLOPE. (10/23/79)



2. GATEHOUSE INTERIOR SHOWING MECHANICAL STOP LOG HOIST. (10/23/79)



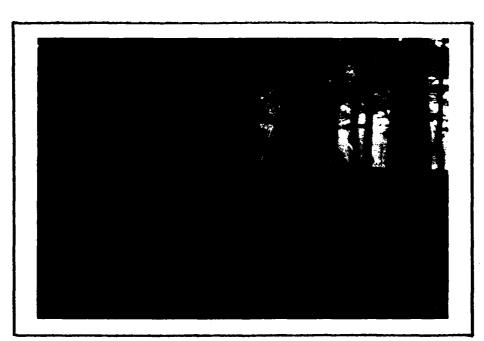
3. INLET PORTAL AND TRASH SCREEN IN GATEHOUSE. (10/23/79)



4. RIPRAP ON UPSTREAM SLOPE, GRASS COVER AND LARGE TREES ON THE DAM. (10/23/79)



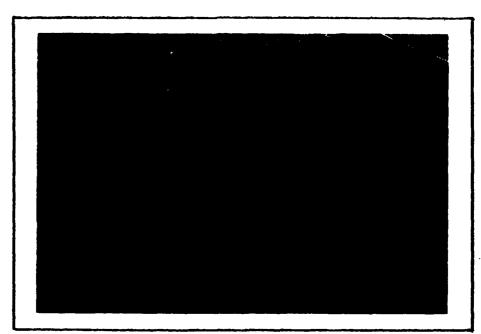
5. CLOSE UP OF LARGE TREES GROWING ON THE DAM CREST AND DOWNSTREAM SLOPE. (10/23/79)



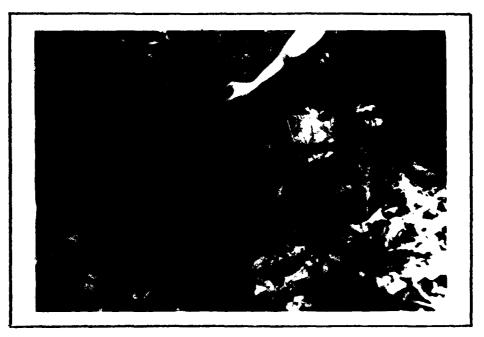
6. DOWNSTREAM SLOPE OF THE DAM SHOWING LARGE TREES AND UNDERGROWTH. (10/23/79)



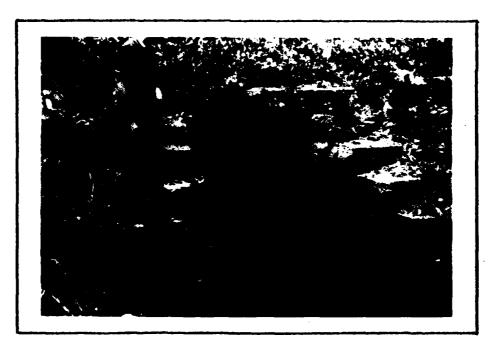
7. 50 FOOT TALL TREES ON THE DAM CREST AND DOWNSTREAM SLOPE. (10/23/79)



8. LARGE TREE ROOT ON THE DAM CREST. (10/23/79)



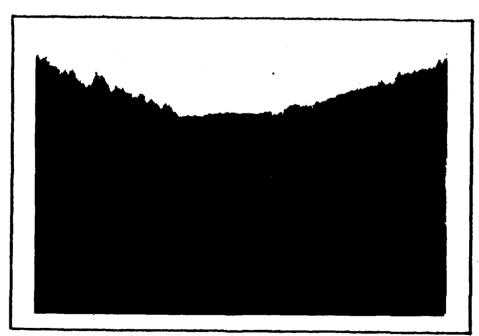
9. OUTLET OF 16 INCH DIAMETER CAST IRON PIPE RESERVOIR BLOW-OFF. (10/23/79)



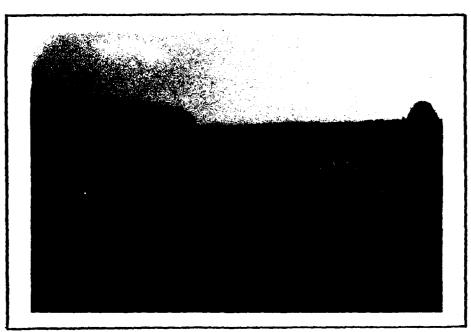
10. OUTLET OF 36 INCH DIAMETER STREAM BY-PASS CONDUIT AT THE DOWN-STREAM TOE OF SLOPE OF THE DAM. (10/23/79)



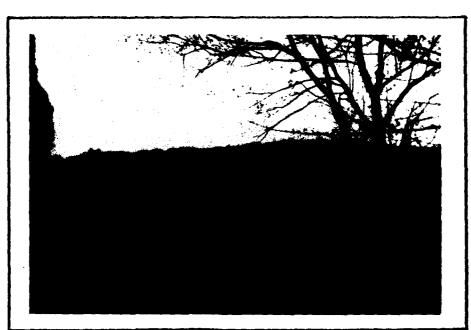
11. 5 G.P.M. SEEPAGE FROM THE DOWNSTREAM TOE OF SLOPE OF THE DAM ALONG THE STREAM BY-PASS OUTLET CHANNEL. (10/23/79)



12. INTAKE CANAL CONNECTING THE AQUEDUCT WITH WESTON RESERVOIR. (10/23/79)



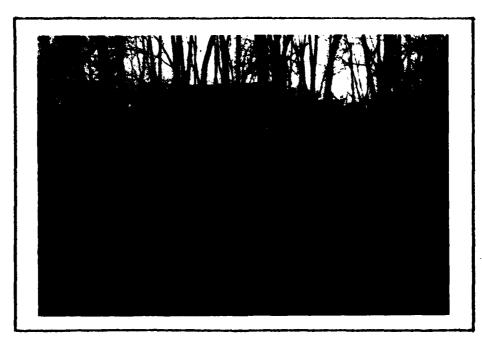
13. WESTON RESERVOIR AS VIEWED FROM WESTON RESERVOIR DAM. (10/23/79)



14. GOLF COURSE THROUGH WHICH DISCHARGE CHANNEL FLOWS FROM APPROXIMATELY 200 TO 900 YARDS DOWNSTREAM OF THE DAM. (10/23/79)



15. POTENTIAL HAZARD AREA ABOUT 1200 YARDS DOWNSTREAM FROM THE DAM. (10/23/79)



16. POTENTIAL HAZARD AREA ABOUT 1400 YARDS DOWNSTREAM FROM THE DAM. (10/23/79)

APPENDIX D

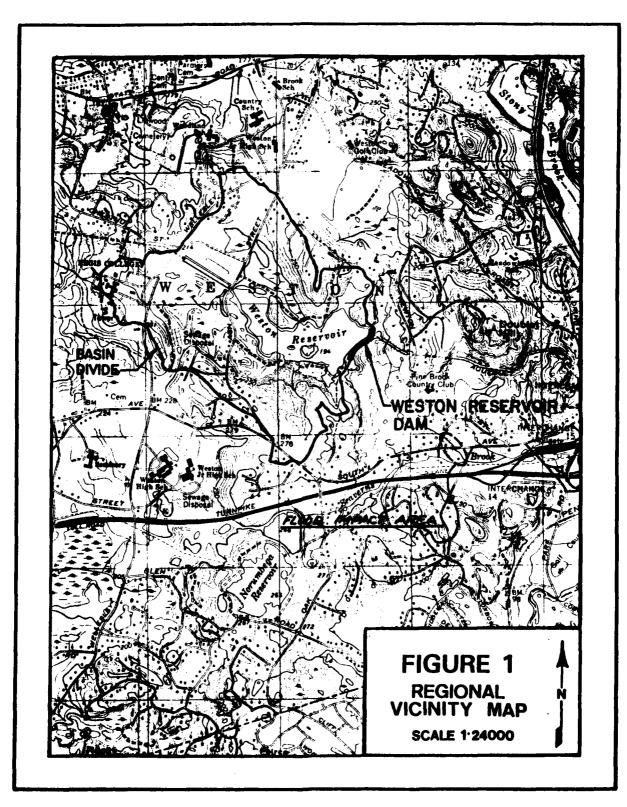
HYDROLOGIC AND HYDRAULIC COMPUTATIONS

APPENDIX D

HYDROLOGIC & HYDRAULIC COMPUTATIONS

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REGIONAL VICINITY MAP, FIGURE 1, SHOWING FLOOD IMPACT AREA	D-1
TP COMPUTATIONS, PMP DATA, ELEV. SKETCH DAM	D-2
STAGE-DISCHARGE DATA, STAGE-STORAGE DATA & SECTION AT HAZARD AREA	D-3
STAGE-STORAGE & STAGE-DISCHARGE CURVES	D-4
HEC-1 DAM SAFETY VERSION, COMPUTER OUTPUT	D-5 to D-9
HEC-1 DAM SAFETY VERSION, BREACH ANALYSIS,	D-10 to D-14



BRYANT ASSOCIATES, INC.
648 Beacon Street
BOSTON, MASSACHUSETTS 02215
(617) 247-1800

JOB	2060	-001	·
			Of
CALCULATED BY	RG		DATE
CHECKED BY	RRB		DATE

WESTON RESERVOIR DAM - H & H

1/2

DRAWAGE AREA

= 0.9 Mi

SNYDER HYDBOGRAPH COEFFICIENTS

Cc = 2.0

Cp = 0.5

TP COMPUTATIONS

L = 1.21 MILES $L_{CA} = 0.61$ MILES $T_P = Q \cdot (L \times L_{CA})^{.3}$

Tp = 2.0 x(1.21x.61). = 2.0 Hoors

PMP DATA

FROM HM5 # 33 THE 24 HOUR 200 SAMI INDEX RAINFALL 16 21.5

Chr. % OF INDEX FOR THIS BASIN = 111

12ht. % " " = 124

24hr. % " " =/33

DAM ELEVATION & LENGTH

L= 1000'

MAG 90 90T

LEV ZO4

C = Z.B TOP OF DAM

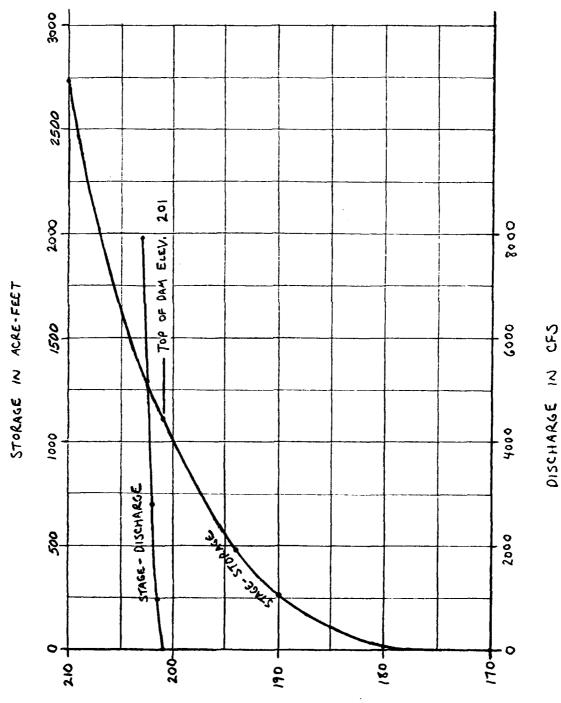
BRYANT ASSOCIATES, INC. 648 Beacon Street BOSTON, MASSACHUSETTS 02215 (617) 247-1800

2060-001	
SHEET NO 0-3	OF
Pt.	DATE
CHECKED BY REB	DATE

2/2 WESTON RESERVOIR DAM - HEH H=0 @ TOP OF DAM CZEST .- ELEVATION = 204.0 MSL $L = 1000' Q = CLH^{1.5}$ c = 2.8TOP OF DAM. STAGE-DISCHARGE ELEVATION HFt. CFS MSL 201 0 0 990 201.5 0.5 2800 202 1.0 5144 202.5 1.5 203 7920 2.0 STAGE - STORAGE CONIC METHOD BY COMPUTER ELEVATION AREA STORAGE MSL Ac. AC. Ft. 170 0 180 190 260 486 NORMAL POOL 194 61 1108 TOP OF DAM 201 120 210 250 2738 HAZARD AREA CROSS-SECTION 125 dist. = 3200 120 Slopes 11.5



SUBJECT	SHEET	BY	DATE	JOB NO
STAGE- STORAGE & STAGE- DISCHARGE CURVES - WESTON	0-4	RRB		2060-001



ELEVATION (FT. ABOVE MSL- NCVD) OF RESERVOIR SURFACE

FLOOD ROUTINGS THROUGH WESTON RESERVOIR LUITHOUT BREACHING

UAM SAFETY VERSION JULY 1978 LAST MUDIFICATION 26 FER 79	2	JULY 1978 26 FER 79	8		INPUT	5			
	₹:			OLUGIC A	NALYSIS	OF WEST	HYDROLUGIC ANALYSIS OF WESTON RESERVOIR DAM	OIR DAM	
v m	A &			NEW ENG	L DAM 1	NSPEC 17	NATIONAL DAM INSPECTION PROGRAM NEW ENGLAND DIVISION - COMPS OF ENGINEERS	ENGINEE	s.
4 10	9 6	200	•	15	•	•	0	•	•
•	י	-	٥	-					
_	5	~	۳.	•	ŝ	9.		60.	¢.
æ	¥	0	WESTON					-	
•	\$			£	FLOW TO	WESTON	INFLOW TO WESTON RESERVOIR		
10	I	-	-	0.0					
Ξ	۵	0	21.5	111	124	133			
75	-							•	0.05
13	7	2.0	6.0						
±	×	-1:1	-0-1	~					
15	¥	-	WESTON					-	
16	ž		POUT	ED OUTFL	ON FROM	WESTON	ROUTED OUTFLOW FROM WESTON RESERVOIR DAM OVERTOPPED	DAM OVE	TOPPED
17	>				-	-			
æ	7	-						-194	7
6	*	201	201.5	202	202.5	203			
20	۲5	0	066	2800	5144	1920			
21	SA	0.0	5.0	55	5	120	250		
25	\$ €	170	180	190	194	201	210		
53	\$\$	201							
5 ¢	30	507							
35	•								

NUN DATED 01/08/80. TIMED 10-18-51.

HYDROLOGIC ANALYSIS OF WESTON RESERVOIR DAM NATIONAL DAM INSPECTION PROGRAM NEW ENGLAND DIVISION - COMPS OF ENGINEERS

0 Ç

NSTAN IPRT IPLT 0 METRC 0 THACE JOB SPECIFICATION LROPT 0 <u>+</u> 0 10AY 0 JOPER 5 NMIN 15 ă o 200 200

RT105= PERCENTAGES OF PMF ROSTED

06. • 80 MULTI-PLAN ANALYSES TO BE PERFOHMED NPLAN= 1 NH 110= 9 LR 110= 1 .30 .40 .50 .60 .70 . •50

1.00

••••••

SUB-AREA RUNOFF COMPUTATION

IAUTO LOCAL INAME ISTAGE ISAME 1 1 SNOW JPRT RAT 10 HYDROGRAPH DATA
THSDA TRSPC
1.90 0.00 INFLOW TO WESTON RESERVOIR IECON ITAPE 0 0 SNAP 0.00 ICOMP 0 IUHG TAREA 1 .90 1STAU WESTON IHYDG 1

896 0.00 872 0.00 R48 0.00 PRECIP DATA SPEE PMS R6 R12 R24 0.00 21.50 111.00 124.00 133.00 TRSPC CUMPUTED BY THE PROGRAM IS .600

ALSMX 0.00 CNSTL .05 LOSS DATA
HTIOL ERAIN STRKS RTIOK STRTL
1.00 0.00 0.00 1.00 0.00 UNIT HYDROGRAPH DATA
TP= 2.00 CP= .50 NI 0L TKR 0.00 STAKE 0.00

LROPT 0

RT10R= 2.00 PECESSION DATA
ORCSN= -.10 -1.70 STRT0=

136. 24. 21. 8. 2.02 HOURS, CP= 137. 1 PH 62 END-OF-PEHIOD OPDINATES, LAG= 2.
43. 94. 86. 120.
103. 94. 86. 31.
16. 15. 13. 12.
6. 6. 6. 5. UNIT HYDROGRAPH 21. 113. 45. 18. 7. 124. 49. 19. 3.

COMP END-OF-PEHIOD FLOM
LOSS COMP O MO.UA HR.MM PERIOD RAIM EXCS LOSS HR.MN PERTOD RAIN EXCS MO.DM SUM 22.66 21.66 1.20 51017. (581.) (551.) (30.) (144.64)

0-6

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ں۔۔۔۔					ROL	TED OU	TFLOW FR	HYDROGHAPH HOUTING ROUTED OUTFLOW FROM WESTON RESERVOIR DAM OVERTOPPED	MYDROGHAPH HOUTING WESTON RESERVOIR (ING IR UAM OV	ERTOPPE	۵		
0					•	1STAU WESTON	1COMP 1	1ECON 0 ROUT	ECON ITAPE 0 0 ROUTING DATA	JPLT	TARC	INAME	INAME ISTAGE	IAUTO 0
C				ಠ	0.0 0.0	0.00.0	AVG 0.00	IRES	1SAME 1	1001	1PMP 0		LSTR	
ပ						NSTPS 1	NSTDL 0	LAG	AMSKK 0.000	0.00°	15K 0.000	STORA -194.	ISPRAT	
L	STAGE	20	201.00		201.50	~	202.00	202.50		3.00 2	STACE	- 0130	203.00 2 STACE- DISCHARGE DATA	DATA
,	FLOW	•	00.0	ŭ.	990.00	28	2800.00	5144.00	_	7920.00	:) ?)	: :
_	SURFACE AREA=	AREA=	÷		•	۶.	52.	61.	120.		(.065			
٦	CAPA	CAPACITY=	:		17.	.•	260.	486.	1108.			46E-5	STAGE-STORAGE DATA	SET SE
	ELEVATION=	1 10N=	170.		180.	•	190.	194.	201.	210.	<u>.</u>			
٠,					CREL 201.0		SP#10 C	COOM EXPW 0.0	PW ELEVL	, coor	CAREA		EXPL 0.0	
								10PEL 201.0	DAM DATA COGD EXP	٥٥	DAMWID 0.			
L	PEAK OUTFLOW IS	SI AO	Ö	4	0. AT TIME	0.0	0.00 HOURS							
J	PEAK OUTFLOW IS	0w 1S	Ó	₹.	O. AT TIME	0.00	0.00 HOURS							
-	PEAK OUTFLOW IS	0W 1S	ō	₹.	D. AT TIME	0.00	0.00 HOURS							
0	PEAK OUTFLOW IS	0w 1S	o	₹.	O. AT TIME	0.0	0.00 HOURS				•			
) _ 	PEAK OUTFLOW IS	SI #0	8	₹ .	18. AT TIME	32.25	32.25 HOURS	å L	ROUTED OUTFLOWS	OUTE	2 2 3			
_	PEAK OUTFLOW IS	S1 40	1.75	٠	271. AT TIME	23.50	23.50 HOURS							
	PEAK OUTFLOW IS	SI #0	535	₹.	535. AT TIME		21.75 HOURS							
	PEAK OUTFLOW IS	0v 1S	803	₹ .	803. AT TIME		21.00 HOURS							
ļ [,]	PEAK QUIFLOW 15	SI 70	1105	4	1105. AT TIME	20.25	20.25 HOURS	_						

0-7

PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-HATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PEW SECUND (CUBIC METERS PER SECOND)
AREA IN SOUARE MILES (SOUARE KILUMETERS)

PERCENTAGES	PEAK INFLOUS - HYDROGHAPH AT WESTON 2.333	SOUTED DUTFLOWS TO WESTON 90
OF PMF	90 1 31 (90 1 3) (
RAT10 1	377.	0.0000
PATIO 2	566.	0.00.0
RATIOS APF RATIO 3	754.	0.001
RATIOS APPLIED TO FLOWS HATIO 3 RATIO 4 RATIO 5 .40 .50 .60	943.	0.00.0
OWS RATIO 5	1131.	18.
RAT10 6	1320.	271.
RAT10 7	1508.	535. 15.16) (
HATIO 8	1697.	
RAT10 9	1885.	1105.

RESULTS OF VARIOUS FLOODS AT MESTON RESERVOIR DAM

SUMMARY OF DAM SAFETY ANALYSIS

CAPACITY		
- MAKIMUM STORAGE	TIME OF FAILURE HOURS	00000000
10P OF DAM 201000 1108: MAY	TIME OF MAX OUTFLOW HOURS	32.25 23.50
	DURATION OVER TOP HOURS	0. 0.00 18. 0.00 19. 0.0
SPILLWAY CREST 201.00 1106.	MAXIMUM OUTFLOW CFS	535:
	MAXIMUM STOPAGE AC-FT	696. 802. 1013. 1169. 1125. 1174. 1156.
INITIAL VALUE 194.00 486.	MAXINUM DEPTH OVER DAM	6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.00
ELEVATION STORAGE OUTFLOA	MAXIMUM RESERVOIR W.S.ELEV	198.12 198.12 198.12 201.01 201.13 201.27 201.61 201.61
PLAN 1	RATIO OF PMF	7EST PLOOD- 1.00

WESTON RESERVOIR DAM BREACH OUTFLOW ROUTED TO DOWNSTREAM DAMAGE AREA

			•								
THIS THE THE THE PARTY OF THE TOTAL	3	JULY 1978 26 FEH 79	T 0 0		31	IN Put					
-	=		,OAH	יטרטיונ	ANBLYSIS	OF WEST	MYDROLDING ANALYSIS OF WESTON HESEMYOIN DAM	M40 410			
~	2 V			NATION	AL UAM 1	WSPECT10	NATIONAL DAM INSPECTION PROGRAM				
m	Ą			Nr K	GLANO DI	- NOISIA	COMPS OF	NEW ENGLAND DIVISION - COMPS OF ENGINEERS			
•	3,	200	0	<u>.</u>	9	0	•	•	0	1	0
·	4	s									
ε	7	~	-	-							
_	ร	.0001	•	•							
Z.	¥	_	MFSTON					_			
,	ĩ		ביי	LO OUTE	LUA FRU	NESTUN	HESERVOIR	HUUTED OUTFLUE FROM WESTUR HESERVOIR DAM OVERTOPPED	CHACAC		
10	>				_			•	2		
11	7	-				1		-201	7		
12	*	201	201.5	202	202.5	203		•	•		
13	۲,	0	037	00 a 2	5144	7920					
*	4	0.0	5.0	55	•	120	250				
15	41 #	170	160	041	151	201	210				
10	4	203									
17	ž	203									•
7	ī	004	0.0	175	c	207	201.5				
2	r	004	0.01	7.	~	201	201				
20	<		7-50					-			
21	₹			-	JAME AFT	Couliss	CHANNEL FOUTTHS TO MAZAND CENTER	CENTER			
25	>				~	-					
23	7	-				•			7		
*2	¥	90.0	40.0	90.0	310	125	3200	0.02			
	17	0	125	330	120	274	119	42H.5	110	431.5	116
25	۲,	*38	119	520	120	400	125				
23	¥	66									

LLOOD HYDHIGHAPH PACKAIG (HEC-1)
LLAN SEETY VEDSION JOUN 1078
LAST MODIFICATION 25 FEB 70

MUM NOTEU A1/29/40. TIMFO 10.14.21. MYTHOLOUIC AMALYSIS OF WESTON MEXEMVOLM DAM NATIONAL DAM INSPECTION PHOGHAM NEW ENGLAND DIVISION - COAPS OF ENGINEERS

NSTAN

AULTI-PLAN ANALYSES TO AE PLHFUNMED NPLAN= 2 NATIO= 1 LATIU= 1

NO INFLOW -> HISS .00

0-11

	•		• • • • • • • • • • • • • • • • • • • •	:	•	••••••		•		:	****
					HAUMO	HYPROHANDH BOUTING)T I NG				
		Ī	UTEU OUI	TFLOW P	404 MEST	MINUTES OUTFLOW FROM MESTING MESFROOTH DAM OVERTOPHED	POIN DAM	UVERTOP	P£0		
			15140 #ESTON	100m	IECON	ISTAG ICOMP IECON ITAPE JPLT JPRT INAME ISTAGE IAUTO 0 0 1 0 0	J.4.C.	TRAU 0	INAME	ISTAGE 0	IAUTO
		01.055 0.0	000-0	0.0.0		ALL PLANS MAVE SAME HOUTIND DATA IMES ISAME IC	SAME A 10PT	- -		LSTR 0	
			NS1PS 1	NSIPS NSTOL	۱. ۸ د د	LAG AVSKK K TSA 0 0.000 0.000 0.000	0.00.0	150		STOKA 15PRAT	
STAGE	201.00	201.50		242.00	202	202.50 243.00 7	7 00.60	•	•	'	
FL04	0.00	00.046		2400.00	5144.00		20.00	STAGE	7920.00 STAGE - DISCHARGE DATA	ROE D	ATA
SURFACE ALEAS	n		5.	.26	61.		۱ ^۲	, , , , , , , , , , , , , , , , , , ,			
CAPACITYE	·.)		17.	240.	• 44.			ر ي. م.	2734. > STAGE- STORAGE DATA	TORAGE	DATA
FLEVATIONE	170.		140.	140.	10.	201.		210.			
		CPEL 201.0		5P+10 0.0	0.0	COG# 1XP# ELFVL 0.0 0.0 0.0		CUUL CA	CAPEA E)	ExPL 0.0	
				•	10P£L		UAM DATA CUGD EAPD DAMBID R.O 0.0 0.	D4M#10			
PERN OUTFLOW IS		0. AT TIME	400. 400. 8400 HUUKS	400.	.01	ОВМ НЧЕВСМ. UBTA 2 ELBM TFAIL •01 175.00 3.00	24,0A14 TFAIL 3.00	WSEL 201.00	FA1LEL 201.50	BREAC No FA	FAILEL BREACH DIMENSIONS-
				44#10	20.	Dam BMEACH DATA 7 ELSM TFAIL 01 175.00 3.00		WSEL 201.00	FA1LEL 201.00	GREACH	PAILEL & BREACH DIMENSIONS-
HFGIN DAM FAILUNE AT 0.00 MUURS	UHE AT 0.01	6 HOURS							3	E E	WITH REFERVOR SUBFACE AT
PEAK OUTFLOW 15		4934. AT TIME		. BB MUUMS						٥	TOP OF DAM

1AUTO 0 157 a GE LS12 0 ISPHAT -1 STORA 0. 17#71 0 1 SX 0 00000 ر تع CHANTEL HOUTING TO HAZAND CENTER 4 15KH 4 0.000 ALL PLANS MAVE SAME MOUTHNE DATA THE TOP HYPAUGHARM HUUTING 1 1 = FE • 1ECON ICOMP 1 AVC 0.00 MSTDL 0 CL USS 0.006 NSTPS 1 0.0 0.0

DRMAL DEPTH CHANNEL MOUTING

EL CHARACTERISTICS
CHANA
POWNSTREAM
SEL SEL
#LNT#
1 C5.0
EL:VT 116.9
004(3)
00+0-
3 ?

	13.54	984.94 18270.56	120.26	84.48 18270.56		
	13 .54	48 .19	11 .79	1521 .61		
	3.10	283.60 12500.75	114.32	263.60		
116.00	1.91	185.32	118.84 123.54	10099.23		
431.50	1.41	123.71	118.37	123.71		
.24.50 116.00	.94 67.78	76.3%	117.86	16.39		
119.00 125.00	.63 53.nu	41.74	117.42	41.74		
574.ELEV.ST3.El 20.00 422.00 20.00 500.00	.35	3301.77	116.95	1d.66 3301.77		
330.00 1	30.97	5.11 2315.56	116.47	5.11 2316.56		
C4NSS SECTION COOPULNATESSTA.ELEV.STA.ELFVFIC 0.00 125.00 330.00 120.00 422.00 119.00 424.50 116.00 431.50 116.00 434.00 119.00 520.00 120.00 500.00 125.00	0.00	0.00	116.00	0.00	7E 15 115.0	E 15 123.3
7	STUDAGE	0U1FL0#	STAGE	707	MAXIMIM STARE 15	MAKIMIJM STARE 15
CHANNEL EROSS-SECTION AT DOWNSTREAM DAMAGE		STAGE - STORAGE AND STAGE - DISCHARGE DATA	FOR THE DOWNSTREAM		٠ ت	1

WESTON RESERVOIR DAM WITHOUT BREACH

SHAMBHY OF DAM SAFETF ANALYSIS

			1417141					
		ELEVATION STUMBLE BUTFLUE	ANTITAL VALUE 201.00 110n.	110 VALUE 1100 1100.	SPILLWAY CMEST 201.00 1108.		100 OF DAM 201.00 1108.	
	RATIO OF PMF	MAAJMUN HESEWOJH W.S.ELEV	TAAIMUM DEPTH OVEH DAM	MARJWUM STUPACE AC-FT	MAA I HUM UUTFLON CF S	DUPATION DVEH TOP HOURS	TIME OF MAK HOTFLOW	TIME OF FAILUME
WESTON PESERVOIR DAM	VOIR BAN	201.00 WITH BREACH	00.0	1104.	•	00.0	00.0	0.00
PLBN 2		ELEVATION STUMBUE OUTFLOW	INITIAL VALUE 201.00 1108.	1at value 201.00 1106.	SHILL AY CHEST 201.00 1104.		TOP UF DAY 201.00 1100.	
	44110 0F:19	MAXIMUM MESFNVJIA 4.5.FLEV	MAAJMUM UEPTH OVEH DAM	PAAJHUM STUMAGE AC-FT	MAAIMUM OUIFLUM CFS	DU4ATION OVER TOP HOUMS	TIME OF MAX BUTFLOW HOURS	TIME OF FAILUNE HOURS
	٥٠.	500.99	0.00	1104.	.434	00.0	40.	00-0
	DOWNST AREA WIT	DOWNSTREAM DAMAGE AREA WITHOUT BREACH	PLay 1	T 14	ST&T10% n	5-5v	:	
			01147	MAAIMUW FLUWACFS	*AXIMUM STAGE*FT	11ME 40U4S		
				.0	110.0	۶.		
	Downs	DOWNSTACAM DAMAGE	2 14 PLA: 3	۸	STATION DS	7-5-		
	3	WITH BREAKING	44110	KAX IMUM FLUM.CFS	MAKIMUM STAUL +FT	TIME HOUMS		
			00•	9631.	151.3	1.00		

4 STREAM RIEWATION AT CHANGE AREA

P-14

APPENDIX E

INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS

